



Short communication

Pseudo-capacitance of composite electrode of ruthenium oxide with porous carbon in non-aqueous electrolyte containing imidazolium salt

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ARTICLE INFO

Article history:

Received 24 September 2009

Received in revised form 6 November 2009

Accepted 11 November 2009

Available online 9 December 2009

Keywords:

Electrochemical capacitor

Pseudo-capacitance

Ruthenium oxide

Non-aqueous electrolyte

Imidazolium salt

ABSTRACT

Pseudo-capacitance of composite materials where ruthenium oxide particles are loaded on activated carbon has been evaluated in the electrolyte of 1-ethyl-3-methyl imidazolium tetrafluoroborate dissolved in acetonitrile. The composite materials prepared by conventional a sol-gel method have dispersed structure of ruthenium oxide particle of tens nanometer diameter on the surface of activated carbon. The extent of the pseudo-capacitance of the composite electrodes in the imidazolium salt electrolyte, estimated by the comparison of the capacitance per surface area of electrode in different non-aqueous electrolyte, is ca. $3\text{--}5\ \mu\text{F cm}^{-2}$ in addition to the double-layer capacitance of ca. $6\ \mu\text{F cm}^{-2}$, depending on the loading status of ruthenium oxide. The symmetric cell consisting of the composite electrode containing 18 wt% of ruthenium oxide and the imidazolium salt electrolyte provides cell capacitance based on the pseudo-capacitance by a constant-current test.

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1. Introduction

Electrochemical capacitors have been attracted as advanced power sources or power assistants with high power density and cycle stability. Many kinds of electrochemical capacitor systems applying with various reactions have been proposed in order to improve the low energy density of double-layer capacitors. Among them, electrochemical capacitors based on ruthenium oxide (RuO_2) electrode has been widely investigated mainly after Zheng et al. reported that hydrated ruthenium oxide ($\text{RuO}_2 \cdot x\text{H}_2\text{O}$) exhibits as a high capacitance as $720\ \text{F g}^{-1}$ in aqueous solution [1–5]. The adsorption process of proton on $\text{RuO}_2 \cdot x\text{H}_2\text{O}$ has been proposed as the origin of the pseudo-capacitance of RuO_2 [1]. The reason for the high capacitance of $\text{RuO}_2 \cdot x\text{H}_2\text{O}$ has been explained as crystalline water in the material also provides active proton and the effective surface of RuO_2 is enlarged [1,6,7].

In most cases the electrolytes used in capacitors based on RuO_2 are aqueous ones, because the above reaction for the pseudo-capacitance of RuO_2 requires proton in electrolyte. Aqueous electrolyte determines the working voltage of a capacitor cell up to ca. 1.2 V and thus limits the energy density of capacitor cell. Therefore some attempts to apply non-aqueous electrolyte to the capacitor based on RuO_2 have been made. Rochefort et al. revealed that ionic liquid containing proton provides pseudo-capacitance of RuO_2 [8]. The authors have proposed non-aqueous polymeric gel

electrolyte, containing $\text{CF}_3\text{SO}_3\text{H}$ dissolved in dimethylformamide and poly(vinylidene difluoride-hexafluoropropylene) matrix, for all-solid-state capacitors based on $\text{RuO}_2 \cdot x\text{H}_2\text{O}$ [9].

Proton itself determines cathodic limit of electrolyte, even if non-aqueous solvent is used. Therefore it is meaningful to find other candidates of cations promoting above adsorption process on RuO_2 . The authors previously reported that 1-ethyl-3-methyl imidazolium tetrafluoroborate (EMIBF_4) can also promote the pseudo-capacitance of crystalline RuO_2 by selecting adequate solvent such as acetonitrile, by the comparative study with tetraethylammonium tetrafluoroborate (TEABF_4) electrolyte [10]. In this sequence EMI cation having hydrogen atoms having tendency to form hydrogen bonding may promote the pseudo-capacitance of RuO_2 . In the previous trial, the obtained specific capacitance was still low insufficient to the practical use, because crystalline RuO_2 with low surface area was used as test electrode. Therefore it should be assessed whether such pseudo-capacitance of RuO_2 provided by EMIBF_4 electrolyte can be utilized in a practical capacitor system. In the present study, the authors have focused on RuO_2 /porous carbon composite electrode, where fine particles of RuO_2 are dispersed on the surface of porous carbon. There have been many attempts to prepare and utilize RuO_2 /carbon composite electrode for capacitors for the purpose of obtaining both high capacitance from RuO_2 and rate capability from carbon substrate with high surface area [11–21]. In addition, the authors would emphasize the necessity of high surface area of RuO_2 fine particles to be applied in non-aqueous capacitor system. The present preliminary study includes the preparation of composite electrodes of RuO_2 with conventional activated carbon (AC) with a conventional

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sol–gel method [1,13], and the evaluation of capacitance of the RuO₂/AC composite electrode in non-aqueous electrolyte containing EMIBF₄.

2. Experimental

2.1. RuO₂/AC electrode preparation

RuO₂/AC composite materials having prescribed RuO₂/AC gravimetric ratios have been prepared by sol–gel method. Activated carbon (AC; capacitor grade) was dispersed into water together with prescribed amount of hydrated ruthenium chloride (RuCl₃·3H₂O) (Kanto Chemical, Japan). An alkali solution was titrated into this suspension and thus ruthenium hydroxide was precipitated. In the present study, two kinds of 1.0 mol dm⁻¹ alkali solutions, sodium hydroxide NaOH and sodium hydrocarbonate NaHCO₃, were applied in order to vary the size of precipitated ruthenium hydroxide. Ruthenium hydroxide/AC composite was collected by the filtration from the resulted suspension. After calcined at 200 °C and dried in a vacuum, resulted RuO₂/AC composites were obtained. The morphology of loaded RuO₂ particles in the composites was observed by transmitted electron microscope (TEM; JEM-2010F, JEOL Co., Japan). The pore structure of the composites was estimated from N₂ adsorption–desorption isotherm (NOVA2000, Quantach Instruments Co., Italy). The content of ruthenium in a RuO₂/AC composite was estimated by comparing the mass of a composite before and after the burning-out of AC at 600 °C for 5 h. For electrochemical measurements, RuO₂/AC composites were molded in sheets with the thickness of ca. 1 mm by the aid of poly(tetrafluoroethylene) (PTFE; Mitsui Fluorochem Co., Japan) binder (10 wt%). Hereafter each composite is denoted with used alkali (OH or HCO) and its RuO₂ content: for example, the composite prepared by using NaHCO₃ and containing 18 wt% of RuO₂ is denoted as RuO₂/AC(HCO, 18).

2.2. Electrolyte preparation

TEABF₄ used in the present study is a commercial material (Tomiya Pure Chemical Co., Japan). EMIBF₄ was prepared by the procedure reported previously [10,22]. Each salt was dissolved into acetonitrile (AN; Synthesis grade, Wako Chemicals, Co., Japan) to 1.0 mol dm⁻³ solution. The dissolving procedure was conducted in a glove box filled with argon. The water content of the electrolytes was checked by a Karl-Fischer titrator (Hiranuma Co., AQ-7) to be in a range from 100 to 200 ppm.

2.3. Measurement of electrochemical properties

For determining the electrochemical properties of RuO₂/AC composites, RuO₂/AC/PTFE composite sheet was cut into a disk, and then fixed with platinum current collector by a PE holder with a screw cap having a hole of 7 mm diameter. A 3-electrode sealed glass cell was assembled with a RuO₂/AC/PTFE composite as working electrode, a silver wire as quasi-reference electrode, and a Pt plate as counter electrode in a glove box filled with argon. Cyclic voltammetry (CV) measurement was conducted by using a potentiostat (HA-151, Hokuto Denko Co., Japan), equipped with a function generator (HB-104, Hokuto Denko Co., Japan) and a digital recorder (8835, Hioki Electric Co., Japan), under the scan rate of 2 mV s⁻¹ between -1.0 V and 0.5 V vs. Ag. The specific capacitances of RuO₂/AC electrodes are estimated from the estimated charge by the voltammograms. The capacitor cell behavior using the RuO₂/AC composites was evaluated by using a 2-electrode symmetric cell. The RuO₂/AC/PTFE composite disks with 7 mm diameter (containing ca. 0.27 g of the composite) were enclosed with a glass fiber cloth separator (Whatman) and small amount of electrolyte

Table 1

Compositions and specific surface areas of RuO₂/AC composites.

	RuO ₂ content expected from starting material/wt%	Estimated RuO ₂ content/wt%	Specific surface area/m ² g ⁻¹
AC	0	0	1173
RuO ₂ /AC(OH, 3)	10	3	1094
RuO ₂ /AC(OH, 18)	20	18	874
RuO ₂ /AC(OH, 34)	40	34	745
RuO ₂ /AC(OH, 42)	50	42	544
RuO ₂ /AC(HCO, 8)	10	8	986
RuO ₂ /AC(HCO, 18)	20	18	957
RuO ₂ /AC(HCO, 32)	40	32	870
RuO ₂ /AC(HCO, 62)	80	62	541

into a sealed cell with platinum current collectors and PTFE body. Constant-current charge–discharge measurement was conducted by using a cycler (BTS-2004, Nagano Co., Japan) under the current of 30 or 150 mA per weight of active material, between 2.0 V and 0 V cut-off voltages.

3. Results and discussion

3.1. Characterization of RuO₂/AC electrodes

The RuO₂ contents and specific surface areas of the RuO₂/AC composites prepared using NaOH and NaHCO₃ solutions are summarized in Table 1. The RuO₂ contents are compared with their expected values from the ratio of starting materials. The estimate RuO₂ content in a composite is always slightly lower than an expected content due to the incompleteness of the precipitation in the sol–gel process; i.e., the ruthenium deposition the wall of glassware, or remain in the solution phase. In both cases, the RuO₂ contents in the composites are more or less assumed to be similar to those expected values except for RuO₂/AC(OH, 42). In the case of some higher loading amount of RuO₂, the incompleteness of the precipitation is not ignorable. The specific surface area of the composite decreases when the RuO₂ content increases, likely due to the covering of pores of AC by RuO₂. For comparable RuO₂ contents, the RuO₂/AC composites prepared by the NaHCO₃ titration have higher specific surface area than those by the NaOH titration. This indicates that RuO₂ particle in the former composites are smaller than the latter.

Fig. 1 shows the TEM images of some RuO₂/AC composites. In all the TEM images, RuO₂ particles are shown as black spots in the AC matrices. The size of RuO₂ particles appears to be varied by the RuO₂ content of composites and the alkali used in the preparation procedure. In the image of RuO₂/AC(OH, 18), RuO₂ particles of ca. 2 nm forming aggregate of ca. tens nanometer are observable. RuO₂ particles in the composite prepared with NaHCO₃ are similar (~2 nm) to those with NaOH but appear to be more dispersed. Such effects are as expected from the previous reports [13]. The smaller particles of RuO₂, and the dispersion of the particles, provide larger specific surface area of RuO₂/AC (HCO) compared with RuO₂/AC(OH).

3.2. Capacitance of RuO₂/AC in imidazolium salt electrolyte

Fig. 2 shows the voltammograms at 3rd cycle of the RuO₂/AC(OH, 18) composite electrode in EMIBF₄/AN and TEABF₄/AN electrolytes. TEABF₄/AN electrolyte provides a typical rectangular voltammogram for a porous polarized electrode. In contrast, the voltammogram in EMIBF₄/AN is somewhat distorted and some feature like broad peaks are found around 0 V and -0.5 V. The apparent charging current of the double-layer in the voltammogram is higher in EMIBF₄/AN than in TEABF₄/AN. Specific

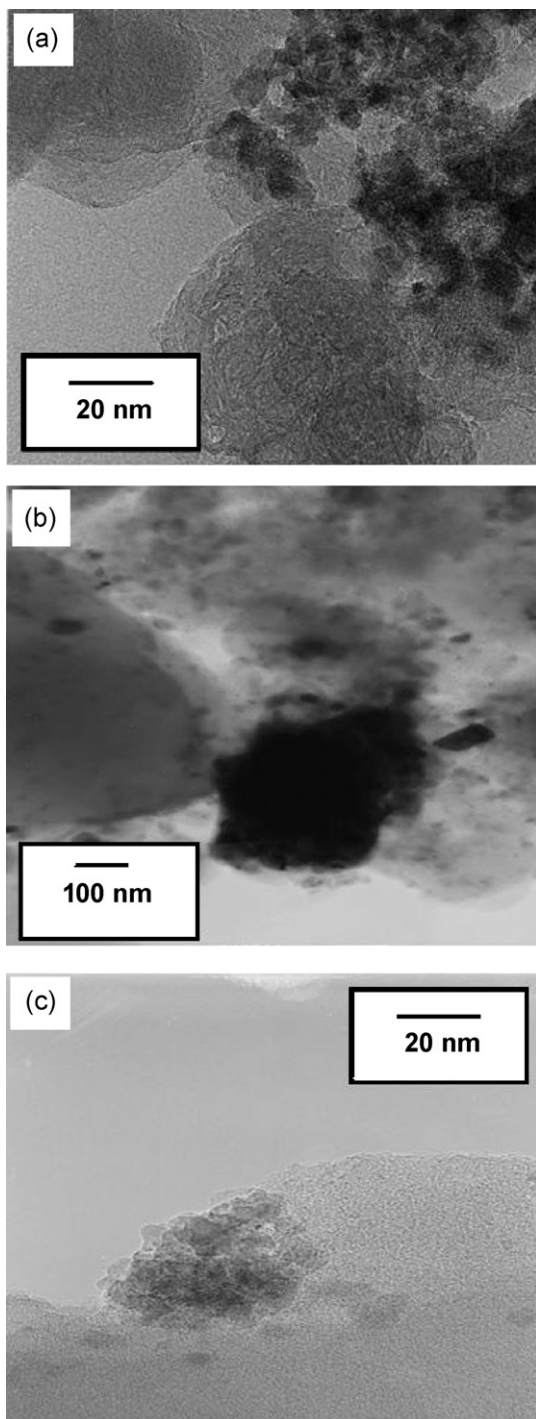


Fig. 1. TEM images of the RuO₂/AC composites. (a) RuO₂/AC(OH, 18); (b) RuO₂/AC(OH, 42); (c) RuO₂/AC(HCO, 18).

capacitances of various RuO₂/AC composites in both electrolytes are estimated from the voltammograms and plotted in Fig. 3 in function of RuO₂ content in the composites. In this figure, specific capacitance values are calculated based on the mass of RuO₂/AC composites except for the case of pristine AC electrode. Pristine AC shows ca. 70 F g⁻¹ of specific capacitance regardless of electrolyte regardless of the kind of electrolyte salt. This capacitance can be assumed to be a double-layer capacitance formed on the carbon surface. For the RuO₂/AC composite electrodes, the capacitance shows different dependence on the RuO₂ content. In TEABF₄/AN, the capacitance monotonously decreases by the

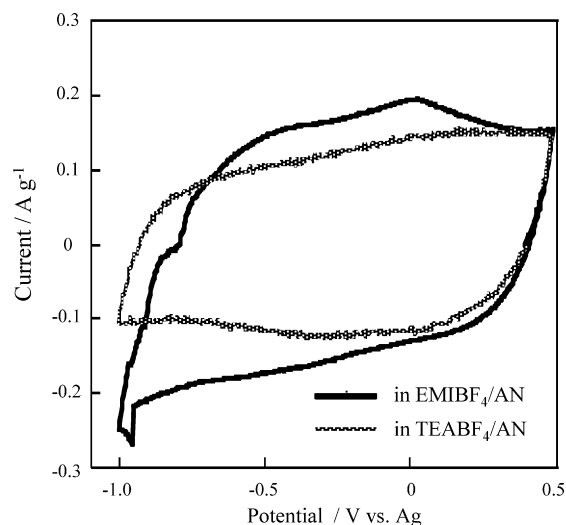


Fig. 2. Cyclic voltammograms of RuO₂/AC(OH, 18) electrode in (a) EMIBF₄/AN and (b) TEABF₄/AN electrolytes.

increase of the RuO₂ content. As shown in Table 1, the surface area of the RuO₂/AC composites decreases by the increase of the RuO₂ content. The decrease of capacitance of the RuO₂/AC electrodes in the TEABF₄/AN electrolyte indicates that the double-layer capacitance mainly contributes in this case. In contrast, the capacitance in EMIBF₄/AN shows a maximum when the RuO₂ content is around 20 wt%, and is higher than that in TEABF₄/AN at the same composite electrode. The higher capacitance of the RuO₂/AC electrodes in EMIBF₄/AN than in TEABF₄/AN, and the existence of the maximum RuO₂ content for the capacitance indicate the existence of an additional capacitance, i.e., pseudo-capacitance, in this electrolyte, similar to crystalline RuO₂ electrode reported previously [10]. The RuO₂/AC(HCO) composites at a loading amount of RuO₂ to 20 wt% exhibit slightly higher capacitances than the RuO₂/AC(OH) composites in the EMIBF₄ electrolyte, probably due to their distributions of smaller RuO₂ particles.

In order to clarify the contribution of pseudo-capacitance, the capacitances by unit surface areas are calculated from the specific capacitance and the specific surface area values. Fig. 3 is rearranged and the dependence of the capacitances per surface area of RuO₂/AC on the RuO₂ content is exhibited in Fig. 4. The capacitance of the

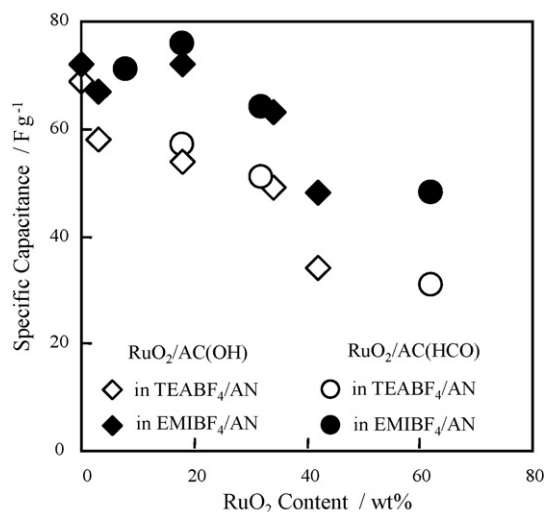


Fig. 3. RuO₂ content dependence of specific capacitance of RuO₂/AC electrodes in EMIBF₄/AN and TEABF₄/AN electrolytes.

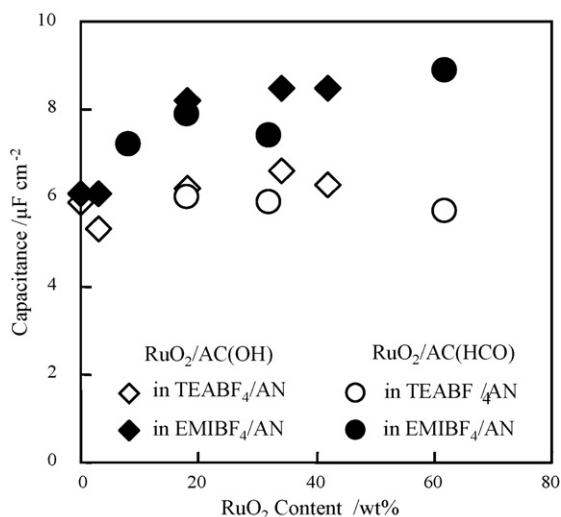


Fig. 4. RuO₂ content dependence of capacitance of RuO₂/AC electrode per surface area in EMIBF₄/AN and TEABF₄/AN.

neat AC electrode is around $6 \mu\text{F cm}^{-2}$ regardless of the electrolyte. In this case only double-layer capacitance on the AC surface exhibits for both the electrolytes. The capacitance values per surface area of RuO₂/AC electrodes are different by the electrolyte. The TEABF₄/AN electrolyte provides the capacitance as high as $6 \mu\text{F cm}^{-2}$, similar to the double-layer capacitance shown on the AC electrode, regardless of the loading amount of RuO₂. In contrast, the capacitances per unit surface area of the RuO₂/AC composite electrodes are above $6 \mu\text{F cm}^{-2}$ and are dependent on the RuO₂ content in the EMIBF₄/AN electrolyte. Such an additional capacitance in this electrolyte is considered to be pseudo-capacitance of RuO₂, as reported previously for crystalline RuO₂ electrode. The dependence of the additional capacitance on the RuO₂ content appears to depend on the preparation method of the RuO₂/AC composite. When the RuO₂/AC is prepared by the titration of NaOH solution, the additional capacitance saturates at the RuO₂ content of ca. 20% and then is stable at ca. $8 \mu\text{F cm}^{-2}$. On the other hand, when the preparation procedure including NaHCO₃ titration is applied, the additional capacitance increases as the increase of the RuO₂ content to 60 wt%. Such a difference in the capacitance behavior for the preparation method of RuO₂/AC electrode may be related with the difference in the morphology of RuO₂ in the composite. The smaller size of RuO₂ particle in the composite may offer the higher reaction interface and then provide rather unsaturated capacitance behavior toward the increase of the RuO₂ content. The calcination temperature of the RuO₂/AC, 200 °C, is expected to provide partially hydrated ruthenium oxide according to the previous study of Zheng and Jow [1]. Nevertheless, the pseudo-capacitance in EMIBF₄/AN electrolyte is dependent on the surface area of ruthenium oxide particle on the composite. The result suggests that the influence of crystalline water is minor and that the adsorption process of EMI cation on ruthenium oxide contribute mainly to the pseudo-capacitance.

A symmetric cell by RuO₂/AC(OH, 18) electrodes with EMIBF₄/AN electrolyte was assembled and evaluated for the cell performance. Fig. 5 shows the voltage profiles of the cell at different cycles in a constant-current test. The cell exhibits typical triangular charge–discharge profiles for capacitor without significant IR drop. The cycle performances, even only at initial stage, of the cell capacitance from such discharge profiles for symmetric cells by AC or RuO₂/AC(OH, 18) electrodes are plotted in Fig. 6. The capacitance for the AC symmetric cell under 30 mA g^{-1} of current decreases from 22 F g^{-1} at initial cycle to 20 F g^{-1} at 30th cycle, probably due to the existence of negligible amount of impurity water in the pores of AC.

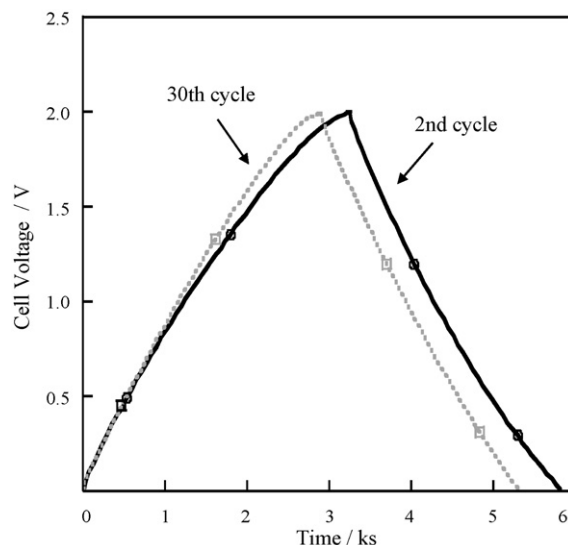


Fig. 5. Constant-current charge–discharge profiles of RuO₂/AC(OH, 18) electrode at 2nd and 30th cycles in EMIBF₄/AN electrolyte. Current density: 30 mA g^{-1} , cut-off voltage: $2.0\text{--}0.1 \text{ V}$.

Such impurity water is considered to affect significantly the electrode behavior only after cycles. The RuO₂/AC cell exhibits rather stable cycle behavior. Such impurity water would be removed after calcination process when preparing the RuO₂/AC composite. Here the authors insist that the pseudo-capacitance based on the interaction between EMIBF₄ and RuO₂ is available under a practical constant-current condition during several tens cycles. Fig. 6 shows the capacitances at two cases of different current densities, 30 mA and 150 mA per weight of active material in either electrode. The capacitance decrease at higher current is more significant at the RuO₂/AC cell compared with the AC cell. This behavior suggests that the slower pseudo-capacitive surface process may be dominant in the capacitance in the RuO₂/AC cell under such a constant-current situation.

From the above results, the RuO₂/AC electrode for this purpose should be designed as nanoparticles of RuO₂ dispersed highly onto porous carbon having adequate pore structure. Future efforts are made for preparing optimum RuO₂/porous carbon composite, and the investigation of cell performances including long-term cycle

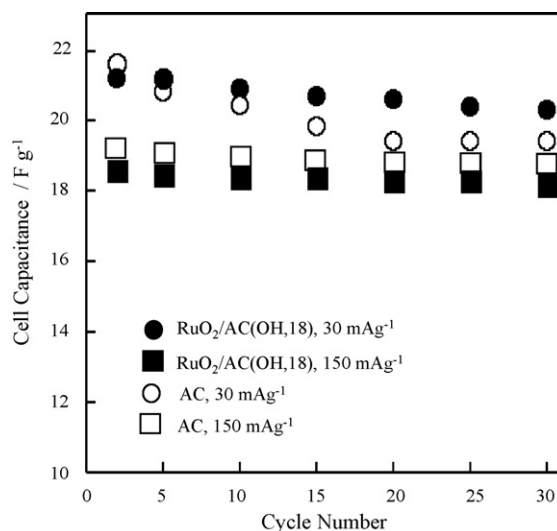


Fig. 6. Cycle performances of specific capacitances of AC and RuO₂/AC(OH, 18) electrodes.

stability. Here it is intended that the pseudo-capacitance of ruthenium oxide electrode by the existence of substituted imidazolium cation has possibility to be extended to electrochemical capacitor system with applicable capacitance.

4. Conclusion

RuO₂/AC composite electrodes exhibit pseudo-capacitance in the EMIBF₄/AN electrolyte. The existence of such pseudo-capacitance is obvious from the dependence of the capacitance per surface area on the RuO₂ content in the composite electrodes. The extent of the pseudo-capacitance is strongly influenced by the loaded content and status, e.g. particle size, of RuO₂. The pseudo-capacitance of the RuO₂/AC electrode is obtained by constant-current test of a symmetric cell as well as by voltammetric test. At the present stage, the increase of the specific capacitance of the RuO₂/AC composite electrode in the EMIBF₄ electrolyte is still small. Further optimization on porous carbon substance and preparation process is inevitable to realize the potential energy density of such RuO₂/carbon composite electrode in the non-aqueous media.

Acknowledgements

The present study is financially supported by Grant-in-Aid for Young Scientists, the Ministry of Education, Culture, Sports, Science and Technology, Japan.

References

- [1] J.P. Zheng, T.R. Jow, *J. Electrochem. Soc.* 142 (1995) L6.
- [2] J.P. Zheng, T.R. Jow, *J. Power Sources* 62 (1996) 155.
- [3] C.-C. Hu, Y.-H. Huang, *J. Electrochem. Soc.* 146 (1999) 2465.
- [4] W. Sugimoto, H. Iwata, Y. Yasukawa, Y. Murakami, Y. Takasu, *Angew. Chem. Int. Ed. Engl.* 42 (2003) 4092.
- [5] W. Sugimoto, H. Iwata, Y. Murakami, Y. Takasu, *J. Electrochem. Soc.* 151 (2004) A1181.
- [6] W. Sugimoto, H. Iwata, K. Yokoshima, Y. Murakami, Y. Takasu, *J. Phys. Chem. B* 109 (2005) 7330.
- [7] O. Barbieri, M. Hahn, A. Foelske, R. Kötz, *J. Electrochem. Soc.* 153 (2006) A2049.
- [8] D. Rochefort, A.-L. Pont, *Electrochem. Commun.* 8 (2006) 1539.
- [9] M. Morita, N. Ohsumi, N. Yoshimoto, M. Egashira, *Electrochemistry* 75 (2007) 641.
- [10] M. Egashira, T. Uno, N. Yoshimoto, M. Morita, *Electrochemistry* 75 (2007) 595.
- [11] J.M. Miller, B. Dunn, T.D. Tran, R.W. Pekala, *J. Electrochem. Soc.* 144 (1997) L309.
- [12] Y. Sato, K. Yomogida, T. Nanaumi, K. Kobayakawa, Y. Ohsawa, M. Kawai, *Electrochem. Solid-State Lett.* 3 (2000) 113.
- [13] H. Kim, B.N. Popov, *J. Power Sources* 104 (2002) 52.
- [14] J.H. Park, J.M. Ko, O.O. Park, *J. Electrochem. Soc.* 150 (2003) A864.
- [15] G. Arabale, D. Wagh, M. Kulkarni, I.S. Mulla, S.P. Vernekar, K. Vijayamohan, A.M. Rao, *Chem. Phys. Lett.* 376 (2003) 207.
- [16] D. Rochefort, C. Hamel, D. Guay, *J. Electrochem. Soc.* 151 (2004) A1141.
- [17] W.-C. Chen, C.-C. Hu, C.-C. Wang, C.-K. Min, *J. Power Sources* 125 (2004) 292.
- [18] C.-C. Hu, W.-C. Chen, *Electrochim. Acta* 49 (2004) 3469.
- [19] I.-H. Kim, J.-H. Kim, K.-B. Kim, *Electrochem. Solid-State Lett.* 8 (2005) A369.
- [20] G.-Y. Yu, W.-X. Chen, Y.-F. Zheng, J. Zhao, X. Li, Z.-D. Xu, *Mater. Lett.* 60 (2006) 2453.
- [21] K. Naoi, S. Ishimoto, N. Ogihara, Y. Nakagawa, S. Hatta, *J. Electrochem. Soc.* 156 (2009) A52.
- [22] M. Egashira, Y. Yamamoto, T. Fukutake, N. Yoshimoto, M. Morita, *J. Fluorine Chem.* 127 (2006) 1261.